

Universidad Carlos III de Madrid

Experimental procedure

Aramid composites have become incressingly important in defence due to their high stiffness lightweight and high energy absorption capacity. The use of personal protections has been

nervased because of the recent rise terrorism, civil and international conflicts since it enables to minimise the morbidity and mortality resulting from ballistic head injuries. Continuum efforts are being dedicated made to reduce further the helnet weight without diminishing addistic resistance. The design of helmets to achieve strictest requirements combining impact

sistance and reasonable weight is currently one of the primary concerns of military and scurity industry. The development of an excellent quality combat belinet involves an expensive and long-time experimental campaign. For this reasons FEM has an important role

in protection development. The principal goal of this work is develop a realistic and validated model of combat belinet to use like a optimize tool for manufacturers. As main contribution, a aultilayer model that contains more than twenty layers that combat helmet are composed is presented. This particularity allowed calculating the damage extension and back-face

Helmet

Ballistically: ballistic limit and curve

(both) and top

Damage: Damage area

with high speed camera

The model replies the different locations that helmet impacted: frontal, rear, lateral

FSP and Sphere projectiles V_{isor} = 600-850 m/s. Impact recorded sequence

Experimental test was performance on plates and combat helmets using different geometries

Combat helmet ballistic validation

Combat helmet damage validation

deformation, validated with computed tomography (CT) scan.

Aramid/PVB ($V_{uex} = 18\%$) $\rho_u = 8.86 \text{ kg/m}^2$

and masses projectiles, in order to calibrate and validate a FEM.

The model provides good correctation with

experimental ballistic limit $V_{expBL} \approx 696 \text{ m/s}$

An analysis of the internal helmet damage after impacts

is carried out through CT scan tomography and

Validation

onto helmet model

Numerical modelling of aramid composite combat helmet under impact threat

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Numerical Model

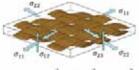
Impact on plates model Symmetry % applicated (b) (b) -1 ···((a) · (b) · (b)

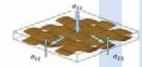
The FEM proposed consists of a multilayer definition where it is possible to observe with good accuracy the different failure modes that appear on composite.

Intra-laminar material model behaviour

In-plane damage

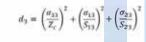
Out of plane damage





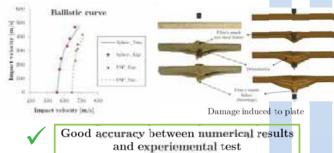
$$d_{f1} = \left(\frac{\sigma_{11}}{\chi_{17}}\right)^{2} + \left(\frac{\sigma_{12}}{S_{12}}\right)^{2} + \left(\frac{\sigma_{13}}{S_{13}}\right)^{2}$$

$$d_{f2} = \left(\frac{\sigma_{22}}{\chi_{27}}\right)^{2} + \left(\frac{\sigma_{12}}{S_{12}}\right)^{2} + \left(\frac{\sigma_{23}}{S_{23}}\right)^{2}$$



Intra-laminar mechanical model behaviour of Aramid/PVB composite was implemented through a VUMAT user subroutine that consider linear elastic behaviour until failure.

Calibration step



In this work, a numerical model for combat helmets of aramid composites against two kinds of ballistic projectiles (1.1g FSP and 1.7g steel sphere) has been developed for

- The numerical model proposed has been calibrated with experimental results on flat plates and then validated ballistically onto real combat helmets.
- The FEM of combat helmet shows very good accuracy on terms of damage variable qualitatively and quantitatively. This is possible to multilayer model proposed in this
- Kinetic energy transference from the projectile produces global deformations/delamination close to the ballistic limit. Far the ballistic limit, damage is more localized.
- An analysis of areal density influence on ballistic limit has been realized. This is a very interesting study because it possible to use this multilayer model like a tool to optimize the number of layers, depending of threat that will be exposed according to different

Areal density influence

compared with numerical simulations

The ballistic limit increase with the areal density and depends of the location of the impact, being lower in lateral impact situations due to the proximity of boundary conditions. This is a very good tool to optimize the number of layers

Conclusions

Acknowledgements

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