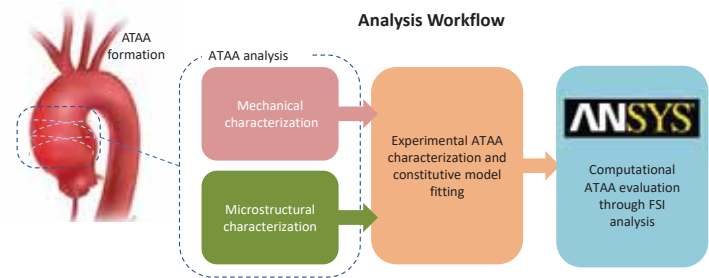


## Introduction

**Introduction:** The microstructure of the aortic tissue influences the mechanical properties of the aorta and it is the main responsible for the onset of pathology of the aneurysm (ATAA) [1]. The presence of collagen fibers within the tissue provides mechanical hyperelasticity and anisotropy. Previous state of art *in-silico* studies considered the Finite Element simulation of ATAA cases through simplified linear elastic or non structurally motivated models [2]. However, a complete analysis of the ATAA tissue has to include both mechanical and microstructural characterization for the definition of a proper constitutive model, which is anisotropic and hyperelastic.

**Aim:** The simultaneous evaluation of the biaxial mechanical properties together with the fiber content of the aortic tissue specimens.

- An experimental setup for the optical and mechanical characterization of ATAA through Small Angle Light Scattering (SALS) [3] and biaxial traction was developed.
- The fitted experimental data were used to reproduce an ATAA case in the *in-silico* FE environment, through a patient case specific Fluid Structure Interaction (FSI) simulation.



## Materials and Methods

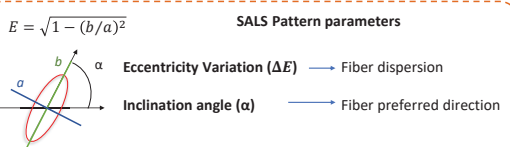
**Experimental setup:** The setup is composed by an optical part responsible for the SALS characterization of the specimen and a mechanical part responsible for the biaxial traction



- Optical components**
- Unpolarized HeNe laser ( $\lambda = 632.8$  nm,  $P = 5$  mW)
  - Broadband dielectric mirror
  - Achromatic doublet focal lens (f. length = 150 mm)

- Mechanical components**
- 4 servo motors
  - 2 load cells (0.1 N accuracy)
  - optical extensometry (0.03 mm/px)
  - 4 pneumatic grippers

**Experimental testing protocol:** Tests performed on 3 healthy and 5 ATAA specimens. Biaxial stresses/stretches and SALS pattern parameters were evaluated at different tension ratios ( $T_{\theta\theta} : T_{zz} = 1:1, 1:0.5, 1:0.75, 0.5:1, 0.75:1$ ). Fiber distributions were evaluated as well, by fitting the SALS patterns through two gaussian functions.

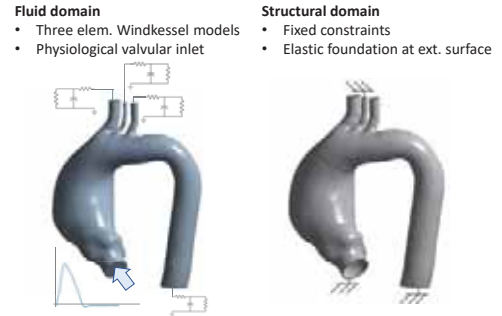


**Data fitting:** The SALS and mechanical data were used to fit a fiber-based constitutive model for the ATAA tissue [4]. The microstructural parameters were evaluated on the basis of fiber distribution from SALS analysis.

$$W = \frac{c}{2}(I_1 - 3) + \frac{k_1}{2k_2} \sum_{i=4,6} \exp([k_2(I_i^*(\phi, k_{ip}, k_{op}) - 1)^2] - 1)$$

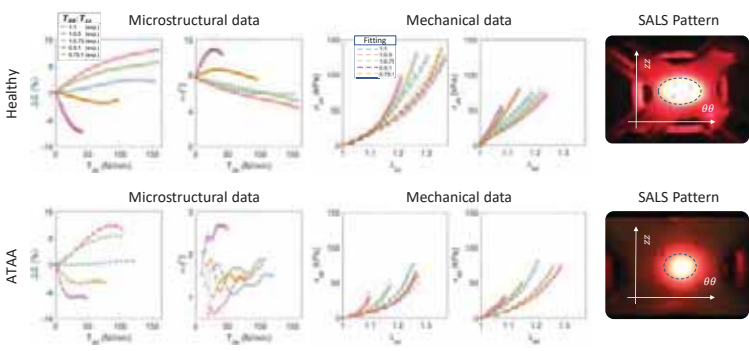


**Computational Finite Element setup:** The experimental data were used for the Finite Element *in-silico* simulation. A one-way FSI simulation was imposed on a patient specific ATAA geometry obtained from CT data segmentation. The fiber based constitutive model was implemented for ANSYS through a custom user defined function developed in FORTRAN.

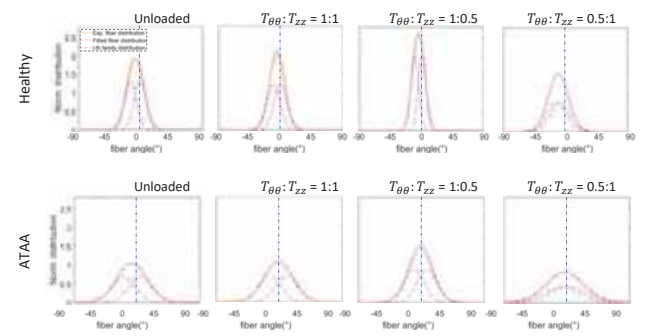


## Results and Discussion

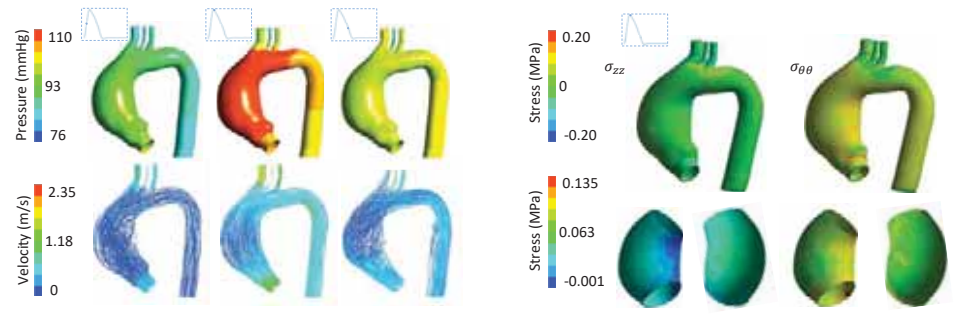
**Constitutive model fitting results:** The constitutive model correctly coped the experimental data according to the constrained fitting ( $R^2 = 0.96$  and  $R^2 = 0.97$  for healthy and ATAA cases)



**Dynamic fiber distribution results:** The ATAA case revealed an higher fiber dispersion in comparison with the healthy case. Sensible differences emerged from the evaluation of distributions according to the different tension states. A strong fiber redistribution occurred at the 1:0.5 and 0.5:1 tension ratios.



**In-silico FE model results:** The fiber-based model was correctly implemented in the FE environment. The hydraulic pressure and flow range were correctly reproduced within the physiological range (110-76 mmHg and 2.35 m/s). The presence of the ATAA bulge produced a sensible pressure drop at systolic peak. The results on the structural domain are reported at systolic pressure maximum. The stress distributions on the structural domain revealed a strong anisotropy. In particular, the circumferential stress exhibited peaks in the inner curvature of the ATAA structure, while the longitudinal stress peaks occurred at the outer curvature area.



## Conclusion

The complete characterization of both healthy and ATAA tissue was assessed through a new experimental setup providing both microstructural and mechanical characterization. The experimental data were interpreted through a fiber-based hyperelastic and anisotropic constitutive model and the dynamical redistribution of the fibers within the biaxially tensioned specimen was assessed. Finally, the fiber-based constitutive model was correctly implemented in the FE environment through the simulation of a given patient specific ATAA case.

[1] Bianchi et al., J of Biomech, 2016  
 [2] Martin et al., Am J Physiol Heart Circ Physiol. 2015  
 [3] Gaul et al., J Mech Behav Biomed Mater, 2017  
 [4] Holzapfel et al., J. Royal Soc. Interface, 2015.